

**Properties of Neon, Magnesium, and Silicon
Primary Cosmic Rays
Results from the Alpha Magnetic Spectrometer
- SUPPLEMENTAL MATERIAL -**

(AMS Collaboration)

For references see the main text.

Detector. — The tracker has nine layers, the first *L1* at the top of the detector, the second *L2* above the magnet, six *L3* to *L8* within the bore of the magnet, and the last *L9* above the ECAL. *L2* to *L8* constitute the inner tracker. Each layer of the tracker provides an independent measurement of the charge Z with a resolution of $\Delta Z/Z = 3\%$ for $Z=10, 12,$ and 14 nuclei. Overall, the inner tracker has a resolution of $\Delta Z/Z = 1.3\%$ for these nuclei. The spatial resolution in each tracker layer is $6.7 \mu\text{m}$ for $Z=10$ nuclei, $7.1 \mu\text{m}$ for $Z=12$ and $7.4 \mu\text{m}$ for $Z=14$. Together, the tracker and the magnet measure the rigidity R of charged cosmic rays, with a maximum detectable rigidity MDR of 3.2 TV for $Z=10$, 3.1 TV for $Z=12$ and 3.0 TV for $Z=14$ over the 3 m lever arm from *L1* to *L9*.

Two of the TOF planes are located above the magnet (upper TOF) and two planes are below the magnet (lower TOF). The overall velocity ($\beta = v/c$) resolution has been measured to be $\Delta(1/\beta) = 0.01$ for $Z=10, 12,$ and 14 nuclei. This discriminates between upward- and downward-going particles. The pulse heights of the two upper planes are combined to provide an independent measurement of the charge with an accuracy $\Delta Z/Z = 2\%$. The pulse heights from the two lower planes are combined to provide another independent charge measurement with the same accuracy.

Results. — Fitting the He, C and O fluxes over the rigidity range 60 GV to 3 TV with Eq. (5) simultaneously with common parameters $s, \gamma, R_0, \Delta\gamma$ yields $C_{\text{He}} = (950 \pm 10) \times 10^{-4} \text{ m}^{-2}\text{sr}^{-1}\text{s}^{-1}\text{GV}^{-1}$, $C_{\text{C}} = (31 \pm 1) \times 10^{-4} \text{ m}^{-2}\text{sr}^{-1}\text{s}^{-1}\text{GV}^{-1}$, $C_{\text{O}} = (33 \pm 1) \times 10^{-4} \text{ m}^{-2}\text{sr}^{-1}\text{s}^{-1}\text{GV}^{-1}$, $\gamma_{\text{HeCO}} = -2.756 \pm 0.002$, $\Delta\gamma = 0.170 \pm 0.015$, $s = 0.05 \pm 0.015$, and $R_0 = 340_{-30}^{+40} \text{ GV}$.

The fit of the normalization parameters $C_{\text{Ne}}, C_{\text{Mg}},$ and C_{Si} was performed on the Ne, Mg, and Si fluxes together with Eq. (5) above 86.5 GV fixing the $\gamma_{\text{NeMgSi}}, \Delta\gamma, s,$ and R_0 parameters. We used the $\Delta\gamma, s,$ and R_0 values obtained from the simultaneous fit to the He, C, and O fluxes and $\gamma_{\text{NeMgSi}} = \gamma_{\text{HeCO}} + \langle\delta\rangle$, where $\langle\delta\rangle = -0.045$ is the average spectral index of Ne/O, Mg/O and Si/O flux ratios above 86.5 GV , see Eq. (4). The fit yields $C_{\text{Ne}} = (5.6 \pm 0.2) \times 10^{-4}$, $C_{\text{Mg}} = (6.7 \pm 0.3) \times 10^{-4}$, and $C_{\text{Si}} = (6.0 \pm 0.3) \times 10^{-4}$ in units of $\text{m}^{-2}\text{sr}^{-1}\text{s}^{-1}\text{GV}^{-1}$.

TABLE SI: The Ne flux Φ as a function of rigidity at the top of AMS in units of $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$ including errors due to statistics (stat.); contributions to the systematic error from the trigger and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

| Rigidity [GV] | Φ | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|---------|-------------------------|------------------------|------------------------|-------------------------|--------------------------|
| 2.15 – 2.40 | (2.371 | 0.013 | 0.094 | 0.052 | 0.012 | 0.108) $\times 10^{-1}$ |
| 2.40 – 2.67 | (2.200 | 0.011 | 0.084 | 0.029 | 0.007 | 0.089) $\times 10^{-1}$ |
| 2.67 – 2.97 | (1.995 | 0.009 | 0.074 | 0.019 | 0.003 | 0.076) $\times 10^{-1}$ |
| 2.97 – 3.29 | (1.800 | 0.008 | 0.065 | 0.015 | 0.001 | 0.067) $\times 10^{-1}$ |
| 3.29 – 3.64 | (1.609 | 0.007 | 0.057 | 0.012 | 0.000 | 0.059) $\times 10^{-1}$ |
| 3.64 – 4.02 | (1.405 | 0.006 | 0.050 | 0.009 | 0.001 | 0.050) $\times 10^{-1}$ |
| 4.02 – 4.43 | (1.210 | 0.005 | 0.042 | 0.007 | 0.001 | 0.043) $\times 10^{-1}$ |
| 4.43 – 4.88 | (1.047 | 0.004 | 0.036 | 0.005 | 0.001 | 0.037) $\times 10^{-1}$ |
| 4.88 – 5.37 | (8.875 | 0.032 | 0.307 | 0.041 | 0.014 | 0.310) $\times 10^{-2}$ |
| 5.37 – 5.90 | (7.490 | 0.027 | 0.258 | 0.031 | 0.014 | 0.260) $\times 10^{-2}$ |
| 5.90 – 6.47 | (6.329 | 0.023 | 0.217 | 0.024 | 0.013 | 0.219) $\times 10^{-2}$ |
| 6.47 – 7.09 | (5.279 | 0.019 | 0.181 | 0.018 | 0.012 | 0.182) $\times 10^{-2}$ |
| 7.09 – 7.76 | (4.341 | 0.015 | 0.149 | 0.013 | 0.010 | 0.150) $\times 10^{-2}$ |
| 7.76 – 8.48 | (3.622 | 0.013 | 0.124 | 0.010 | 0.009 | 0.125) $\times 10^{-2}$ |
| 8.48 – 9.26 | (3.017 | 0.011 | 0.103 | 0.008 | 0.008 | 0.104) $\times 10^{-2}$ |
| 9.26 – 10.1 | (2.449 | 0.009 | 0.084 | 0.006 | 0.007 | 0.084) $\times 10^{-2}$ |
| 10.1 – 11.0 | (2.013 | 0.008 | 0.069 | 0.005 | 0.006 | 0.069) $\times 10^{-2}$ |
| 11.0 – 12.0 | (1.653 | 0.007 | 0.057 | 0.004 | 0.005 | 0.057) $\times 10^{-2}$ |
| 12.0 – 13.0 | (1.339 | 0.006 | 0.046 | 0.003 | 0.004 | 0.046) $\times 10^{-2}$ |
| 13.0 – 14.1 | (1.108 | 0.005 | 0.038 | 0.002 | 0.004 | 0.038) $\times 10^{-2}$ |
| 14.1 – 15.3 | (9.052 | 0.042 | 0.310 | 0.020 | 0.030 | 0.312) $\times 10^{-3}$ |
| 15.3 – 16.6 | (7.356 | 0.036 | 0.252 | 0.016 | 0.025 | 0.254) $\times 10^{-3}$ |
| 16.6 – 18.0 | (6.074 | 0.031 | 0.208 | 0.014 | 0.021 | 0.210) $\times 10^{-3}$ |
| 18.0 – 19.5 | (4.997 | 0.026 | 0.171 | 0.012 | 0.017 | 0.172) $\times 10^{-3}$ |
| 19.5 – 21.1 | (4.047 | 0.022 | 0.139 | 0.010 | 0.014 | 0.140) $\times 10^{-3}$ |
| 21.1 – 22.8 | (3.341 | 0.018 | 0.115 | 0.009 | 0.012 | 0.116) $\times 10^{-3}$ |
| 22.8 – 24.7 | (2.760 | 0.015 | 0.095 | 0.008 | 0.010 | 0.095) $\times 10^{-3}$ |
| 24.7 – 26.7 | (2.237 | 0.013 | 0.077 | 0.007 | 0.008 | 0.077) $\times 10^{-3}$ |
| 26.7 – 28.8 | (1.845 | 0.011 | 0.063 | 0.006 | 0.007 | 0.064) $\times 10^{-3}$ |
| 28.8 – 31.1 | (1.486 | 0.009 | 0.051 | 0.005 | 0.006 | 0.052) $\times 10^{-3}$ |
| 31.1 – 33.5 | (1.226 | 0.008 | 0.042 | 0.004 | 0.005 | 0.043) $\times 10^{-3}$ |
| 33.5 – 36.1 | (1.019 | 0.007 | 0.035 | 0.004 | 0.004 | 0.035) $\times 10^{-3}$ |
| 36.1 – 38.9 | (8.259 | 0.060 | 0.284 | 0.033 | 0.033 | 0.288) $\times 10^{-4}$ |
| 38.9 – 41.9 | (6.901 | 0.053 | 0.237 | 0.028 | 0.028 | 0.241) $\times 10^{-4}$ |
| 41.9 – 45.1 | (5.668 | 0.046 | 0.195 | 0.024 | 0.023 | 0.198) $\times 10^{-4}$ |
| 45.1 – 48.5 | (4.627 | 0.040 | 0.159 | 0.021 | 0.019 | 0.162) $\times 10^{-4}$ |
| 48.5 – 52.2 | (3.830 | 0.035 | 0.132 | 0.018 | 0.016 | 0.134) $\times 10^{-4}$ |
| 52.2 – 56.1 | (3.163 | 0.031 | 0.109 | 0.015 | 0.014 | 0.111) $\times 10^{-4}$ |

Table continued

TABLE SI – (Continued).

| Rigidity [GV] | Φ | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|---------|-------------------------|------------------------|------------------------|-------------------------|--------------------------|
| 56.1 – 60.3 | (2.582 | 0.027 | 0.089 | 0.013 | 0.011 | 0.091) $\times 10^{-4}$ |
| 60.3 – 64.8 | (2.104 | 0.024 | 0.073 | 0.011 | 0.010 | 0.074) $\times 10^{-4}$ |
| 64.8 – 69.7 | (1.746 | 0.021 | 0.060 | 0.009 | 0.008 | 0.062) $\times 10^{-4}$ |
| 69.7 – 74.9 | (1.429 | 0.018 | 0.049 | 0.008 | 0.007 | 0.050) $\times 10^{-4}$ |
| 74.9 – 80.5 | (1.185 | 0.016 | 0.041 | 0.007 | 0.006 | 0.042) $\times 10^{-4}$ |
| 80.5 – 86.5 | (9.599 | 0.138 | 0.332 | 0.054 | 0.048 | 0.340) $\times 10^{-5}$ |
| 86.5 – 93.0 | (7.880 | 0.120 | 0.273 | 0.045 | 0.041 | 0.280) $\times 10^{-5}$ |
| 93.0 – 100 | (6.402 | 0.104 | 0.222 | 0.037 | 0.034 | 0.228) $\times 10^{-5}$ |
| 100 – 108 | (5.217 | 0.088 | 0.181 | 0.031 | 0.029 | 0.186) $\times 10^{-5}$ |
| 108 – 116 | (4.183 | 0.079 | 0.145 | 0.025 | 0.024 | 0.149) $\times 10^{-5}$ |
| 116 – 125 | (3.520 | 0.068 | 0.122 | 0.021 | 0.021 | 0.126) $\times 10^{-5}$ |
| 125 – 135 | (2.825 | 0.058 | 0.098 | 0.017 | 0.017 | 0.101) $\times 10^{-5}$ |
| 135 – 147 | (2.327 | 0.048 | 0.081 | 0.014 | 0.015 | 0.083) $\times 10^{-5}$ |
| 147 – 160 | (1.749 | 0.040 | 0.061 | 0.010 | 0.012 | 0.063) $\times 10^{-5}$ |
| 160 – 175 | (1.354 | 0.033 | 0.047 | 0.008 | 0.009 | 0.049) $\times 10^{-5}$ |
| 175 – 192 | (1.069 | 0.027 | 0.037 | 0.006 | 0.008 | 0.039) $\times 10^{-5}$ |
| 192 – 211 | (8.396 | 0.228 | 0.293 | 0.051 | 0.066 | 0.305) $\times 10^{-6}$ |
| 211 – 233 | (6.460 | 0.186 | 0.226 | 0.041 | 0.054 | 0.236) $\times 10^{-6}$ |
| 233 – 259 | (5.000 | 0.150 | 0.175 | 0.033 | 0.045 | 0.184) $\times 10^{-6}$ |
| 259 – 291 | (3.527 | 0.114 | 0.124 | 0.025 | 0.035 | 0.131) $\times 10^{-6}$ |
| 291 – 330 | (2.643 | 0.089 | 0.093 | 0.020 | 0.029 | 0.099) $\times 10^{-6}$ |
| 330 – 379 | (1.885 | 0.067 | 0.067 | 0.016 | 0.023 | 0.072) $\times 10^{-6}$ |
| 379 – 441 | (1.248 | 0.049 | 0.044 | 0.012 | 0.017 | 0.049) $\times 10^{-6}$ |
| 441 – 525 | (8.288 | 0.341 | 0.296 | 0.099 | 0.133 | 0.339) $\times 10^{-7}$ |
| 525 – 660 | (4.684 | 0.202 | 0.169 | 0.070 | 0.093 | 0.205) $\times 10^{-7}$ |
| 660 – 860 | (2.419 | 0.120 | 0.089 | 0.047 | 0.063 | 0.119) $\times 10^{-7}$ |
| 860 – 1200 | (1.187 | 0.065 | 0.045 | 0.032 | 0.044 | 0.070) $\times 10^{-7}$ |
| 1200 – 3000 | (2.791 | 0.338 | 0.131 | 0.048 | 0.137 | 0.196) $\times 10^{-8}$ |

TABLE SII: The Mg flux Φ as a function of rigidity at the top of AMS in units of $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$ including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

| Rigidity [GV] | Φ | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|---------|-------------------------|------------------------|------------------------|-------------------------|--------------------------|
| 2.15 – 2.40 | (3.081 | 0.015 | 0.126 | 0.039 | 0.015 | 0.132) $\times 10^{-1}$ |
| 2.40 – 2.67 | (2.808 | 0.012 | 0.110 | 0.033 | 0.009 | 0.115) $\times 10^{-1}$ |
| 2.67 – 2.97 | (2.492 | 0.010 | 0.095 | 0.026 | 0.004 | 0.099) $\times 10^{-1}$ |
| 2.97 – 3.29 | (2.193 | 0.009 | 0.082 | 0.020 | 0.002 | 0.084) $\times 10^{-1}$ |
| 3.29 – 3.64 | (1.951 | 0.007 | 0.072 | 0.016 | 0.000 | 0.073) $\times 10^{-1}$ |
| 3.64 – 4.02 | (1.692 | 0.006 | 0.061 | 0.012 | 0.001 | 0.063) $\times 10^{-1}$ |
| 4.02 – 4.43 | (1.462 | 0.005 | 0.053 | 0.010 | 0.001 | 0.053) $\times 10^{-1}$ |
| 4.43 – 4.88 | (1.251 | 0.004 | 0.045 | 0.007 | 0.002 | 0.045) $\times 10^{-1}$ |
| 4.88 – 5.37 | (1.070 | 0.003 | 0.038 | 0.006 | 0.002 | 0.038) $\times 10^{-1}$ |
| 5.37 – 5.90 | (9.028 | 0.029 | 0.320 | 0.042 | 0.017 | 0.323) $\times 10^{-2}$ |
| 5.90 – 6.47 | (7.503 | 0.024 | 0.265 | 0.032 | 0.016 | 0.268) $\times 10^{-2}$ |
| 6.47 – 7.09 | (6.266 | 0.020 | 0.221 | 0.024 | 0.014 | 0.223) $\times 10^{-2}$ |
| 7.09 – 7.76 | (5.204 | 0.016 | 0.184 | 0.018 | 0.013 | 0.185) $\times 10^{-2}$ |
| 7.76 – 8.48 | (4.307 | 0.014 | 0.152 | 0.014 | 0.011 | 0.153) $\times 10^{-2}$ |
| 8.48 – 9.26 | (3.546 | 0.011 | 0.125 | 0.011 | 0.010 | 0.126) $\times 10^{-2}$ |
| 9.26 – 10.1 | (2.914 | 0.010 | 0.103 | 0.009 | 0.008 | 0.103) $\times 10^{-2}$ |
| 10.1 – 11.0 | (2.402 | 0.008 | 0.085 | 0.007 | 0.007 | 0.085) $\times 10^{-2}$ |
| 11.0 – 12.0 | (1.953 | 0.007 | 0.069 | 0.005 | 0.006 | 0.069) $\times 10^{-2}$ |
| 12.0 – 13.0 | (1.602 | 0.006 | 0.056 | 0.004 | 0.005 | 0.057) $\times 10^{-2}$ |
| 13.0 – 14.1 | (1.320 | 0.005 | 0.046 | 0.004 | 0.004 | 0.047) $\times 10^{-2}$ |
| 14.1 – 15.3 | (1.091 | 0.005 | 0.038 | 0.003 | 0.004 | 0.039) $\times 10^{-2}$ |
| 15.3 – 16.6 | (8.924 | 0.039 | 0.314 | 0.025 | 0.030 | 0.317) $\times 10^{-3}$ |
| 16.6 – 18.0 | (7.279 | 0.033 | 0.256 | 0.020 | 0.025 | 0.258) $\times 10^{-3}$ |
| 18.0 – 19.5 | (5.992 | 0.028 | 0.211 | 0.017 | 0.021 | 0.213) $\times 10^{-3}$ |
| 19.5 – 21.1 | (4.872 | 0.024 | 0.172 | 0.015 | 0.017 | 0.173) $\times 10^{-3}$ |
| 21.1 – 22.8 | (3.984 | 0.020 | 0.140 | 0.012 | 0.014 | 0.142) $\times 10^{-3}$ |
| 22.8 – 24.7 | (3.259 | 0.016 | 0.115 | 0.011 | 0.012 | 0.116) $\times 10^{-3}$ |
| 24.7 – 26.7 | (2.665 | 0.014 | 0.094 | 0.009 | 0.010 | 0.095) $\times 10^{-3}$ |
| 26.7 – 28.8 | (2.189 | 0.012 | 0.077 | 0.008 | 0.008 | 0.078) $\times 10^{-3}$ |
| 28.8 – 31.1 | (1.809 | 0.010 | 0.064 | 0.007 | 0.007 | 0.065) $\times 10^{-3}$ |
| 31.1 – 33.5 | (1.488 | 0.009 | 0.053 | 0.006 | 0.006 | 0.053) $\times 10^{-3}$ |
| 33.5 – 36.1 | (1.225 | 0.007 | 0.043 | 0.005 | 0.005 | 0.044) $\times 10^{-3}$ |
| 36.1 – 38.9 | (1.004 | 0.006 | 0.036 | 0.004 | 0.004 | 0.036) $\times 10^{-3}$ |
| 38.9 – 41.9 | (8.113 | 0.056 | 0.287 | 0.035 | 0.033 | 0.291) $\times 10^{-4}$ |
| 41.9 – 45.1 | (6.826 | 0.050 | 0.242 | 0.030 | 0.028 | 0.246) $\times 10^{-4}$ |
| 45.1 – 48.5 | (5.534 | 0.043 | 0.197 | 0.025 | 0.023 | 0.199) $\times 10^{-4}$ |
| 48.5 – 52.2 | (4.567 | 0.038 | 0.162 | 0.021 | 0.019 | 0.165) $\times 10^{-4}$ |
| 52.2 – 56.1 | (3.752 | 0.033 | 0.134 | 0.018 | 0.016 | 0.136) $\times 10^{-4}$ |

Table continued

TABLE SII – (Continued).

| Rigidity [GV] | Φ | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|---------|-------------------------|------------------------|------------------------|-------------------------|--------------------------|
| 56.1 – 60.3 | (3.096 | 0.029 | 0.110 | 0.015 | 0.014 | 0.112) $\times 10^{-4}$ |
| 60.3 – 64.8 | (2.532 | 0.026 | 0.090 | 0.013 | 0.011 | 0.092) $\times 10^{-4}$ |
| 64.8 – 69.7 | (2.076 | 0.022 | 0.074 | 0.011 | 0.010 | 0.076) $\times 10^{-4}$ |
| 69.7 – 74.9 | (1.714 | 0.019 | 0.061 | 0.009 | 0.008 | 0.063) $\times 10^{-4}$ |
| 74.9 – 80.5 | (1.369 | 0.017 | 0.049 | 0.007 | 0.007 | 0.050) $\times 10^{-4}$ |
| 80.5 – 86.5 | (1.157 | 0.015 | 0.042 | 0.006 | 0.006 | 0.042) $\times 10^{-4}$ |
| 86.5 – 93.0 | (9.427 | 0.129 | 0.339 | 0.050 | 0.049 | 0.346) $\times 10^{-5}$ |
| 93.0 – 100 | (7.783 | 0.113 | 0.280 | 0.042 | 0.041 | 0.286) $\times 10^{-5}$ |
| 100 – 108 | (6.223 | 0.095 | 0.224 | 0.033 | 0.034 | 0.229) $\times 10^{-5}$ |
| 108 – 116 | (5.199 | 0.086 | 0.187 | 0.028 | 0.029 | 0.192) $\times 10^{-5}$ |
| 116 – 125 | (4.263 | 0.074 | 0.154 | 0.022 | 0.025 | 0.157) $\times 10^{-5}$ |
| 125 – 135 | (3.465 | 0.063 | 0.125 | 0.018 | 0.021 | 0.128) $\times 10^{-5}$ |
| 135 – 147 | (2.736 | 0.051 | 0.099 | 0.014 | 0.017 | 0.101) $\times 10^{-5}$ |
| 147 – 160 | (2.154 | 0.044 | 0.078 | 0.011 | 0.014 | 0.080) $\times 10^{-5}$ |
| 160 – 175 | (1.673 | 0.036 | 0.061 | 0.009 | 0.012 | 0.062) $\times 10^{-5}$ |
| 175 – 192 | (1.295 | 0.030 | 0.047 | 0.007 | 0.009 | 0.048) $\times 10^{-5}$ |
| 192 – 211 | (1.025 | 0.025 | 0.037 | 0.006 | 0.008 | 0.039) $\times 10^{-5}$ |
| 211 – 233 | (7.857 | 0.203 | 0.286 | 0.044 | 0.065 | 0.297) $\times 10^{-6}$ |
| 233 – 259 | (5.952 | 0.162 | 0.217 | 0.036 | 0.054 | 0.227) $\times 10^{-6}$ |
| 259 – 291 | (4.305 | 0.125 | 0.158 | 0.028 | 0.043 | 0.166) $\times 10^{-6}$ |
| 291 – 330 | (3.247 | 0.098 | 0.119 | 0.024 | 0.036 | 0.127) $\times 10^{-6}$ |
| 330 – 379 | (2.179 | 0.072 | 0.080 | 0.019 | 0.027 | 0.087) $\times 10^{-6}$ |
| 379 – 441 | (1.416 | 0.051 | 0.053 | 0.015 | 0.020 | 0.058) $\times 10^{-6}$ |
| 441 – 525 | (9.378 | 0.360 | 0.350 | 0.120 | 0.159 | 0.403) $\times 10^{-7}$ |
| 525 – 660 | (6.083 | 0.229 | 0.230 | 0.100 | 0.129 | 0.282) $\times 10^{-7}$ |
| 660 – 860 | (2.841 | 0.129 | 0.109 | 0.063 | 0.080 | 0.149) $\times 10^{-7}$ |
| 860 – 1200 | (1.385 | 0.069 | 0.055 | 0.043 | 0.055 | 0.089) $\times 10^{-7}$ |
| 1200 – 3000 | (2.529 | 0.320 | 0.120 | 0.049 | 0.151 | 0.199) $\times 10^{-8}$ |

TABLE III: The Si flux Φ as a function of rigidity at the top of AMS in units of $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$ including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

| Rigidity [GV] | Φ | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|---------|-------------------------|------------------------|------------------------|-------------------------|--------------------------|
| 2.15 – 2.40 | (2.172 | 0.013 | 0.093 | 0.102 | 0.011 | 0.138) $\times 10^{-1}$ |
| 2.40 – 2.67 | (2.012 | 0.011 | 0.083 | 0.046 | 0.006 | 0.095) $\times 10^{-1}$ |
| 2.67 – 2.97 | (1.826 | 0.009 | 0.073 | 0.023 | 0.003 | 0.076) $\times 10^{-1}$ |
| 2.97 – 3.29 | (1.635 | 0.008 | 0.064 | 0.018 | 0.001 | 0.066) $\times 10^{-1}$ |
| 3.29 – 3.64 | (1.454 | 0.006 | 0.056 | 0.014 | 0.000 | 0.057) $\times 10^{-1}$ |
| 3.64 – 4.02 | (1.263 | 0.005 | 0.048 | 0.010 | 0.001 | 0.049) $\times 10^{-1}$ |
| 4.02 – 4.43 | (1.085 | 0.004 | 0.041 | 0.008 | 0.001 | 0.041) $\times 10^{-1}$ |
| 4.43 – 4.88 | (9.373 | 0.037 | 0.349 | 0.060 | 0.012 | 0.355) $\times 10^{-2}$ |
| 4.88 – 5.37 | (7.906 | 0.030 | 0.293 | 0.046 | 0.013 | 0.297) $\times 10^{-2}$ |
| 5.37 – 5.90 | (6.637 | 0.025 | 0.246 | 0.035 | 0.012 | 0.248) $\times 10^{-2}$ |
| 5.90 – 6.47 | (5.656 | 0.021 | 0.209 | 0.027 | 0.012 | 0.211) $\times 10^{-2}$ |
| 6.47 – 7.09 | (4.721 | 0.017 | 0.174 | 0.021 | 0.011 | 0.176) $\times 10^{-2}$ |
| 7.09 – 7.76 | (3.977 | 0.014 | 0.147 | 0.016 | 0.010 | 0.148) $\times 10^{-2}$ |
| 7.76 – 8.48 | (3.251 | 0.012 | 0.120 | 0.013 | 0.008 | 0.121) $\times 10^{-2}$ |
| 8.48 – 9.26 | (2.717 | 0.010 | 0.100 | 0.010 | 0.007 | 0.101) $\times 10^{-2}$ |
| 9.26 – 10.1 | (2.247 | 0.009 | 0.083 | 0.008 | 0.006 | 0.083) $\times 10^{-2}$ |
| 10.1 – 11.0 | (1.859 | 0.007 | 0.069 | 0.006 | 0.005 | 0.069) $\times 10^{-2}$ |
| 11.0 – 12.0 | (1.523 | 0.006 | 0.056 | 0.005 | 0.005 | 0.057) $\times 10^{-2}$ |
| 12.0 – 13.0 | (1.260 | 0.006 | 0.046 | 0.004 | 0.004 | 0.047) $\times 10^{-2}$ |
| 13.0 – 14.1 | (1.046 | 0.005 | 0.039 | 0.003 | 0.003 | 0.039) $\times 10^{-2}$ |
| 14.1 – 15.3 | (8.551 | 0.041 | 0.315 | 0.027 | 0.028 | 0.318) $\times 10^{-3}$ |
| 15.3 – 16.6 | (7.036 | 0.035 | 0.260 | 0.022 | 0.024 | 0.262) $\times 10^{-3}$ |
| 16.6 – 18.0 | (5.759 | 0.030 | 0.213 | 0.018 | 0.020 | 0.214) $\times 10^{-3}$ |
| 18.0 – 19.5 | (4.735 | 0.025 | 0.175 | 0.015 | 0.017 | 0.176) $\times 10^{-3}$ |
| 19.5 – 21.1 | (3.916 | 0.021 | 0.145 | 0.012 | 0.014 | 0.146) $\times 10^{-3}$ |
| 21.1 – 22.8 | (3.200 | 0.018 | 0.118 | 0.010 | 0.012 | 0.119) $\times 10^{-3}$ |
| 22.8 – 24.7 | (2.623 | 0.015 | 0.097 | 0.008 | 0.010 | 0.098) $\times 10^{-3}$ |
| 24.7 – 26.7 | (2.171 | 0.013 | 0.080 | 0.007 | 0.008 | 0.081) $\times 10^{-3}$ |
| 26.7 – 28.8 | (1.799 | 0.011 | 0.067 | 0.006 | 0.007 | 0.067) $\times 10^{-3}$ |
| 28.8 – 31.1 | (1.487 | 0.009 | 0.055 | 0.005 | 0.006 | 0.056) $\times 10^{-3}$ |
| 31.1 – 33.5 | (1.231 | 0.008 | 0.046 | 0.004 | 0.005 | 0.046) $\times 10^{-3}$ |
| 33.5 – 36.1 | (1.012 | 0.007 | 0.038 | 0.003 | 0.004 | 0.038) $\times 10^{-3}$ |
| 36.1 – 38.9 | (8.446 | 0.060 | 0.313 | 0.029 | 0.034 | 0.317) $\times 10^{-4}$ |
| 38.9 – 41.9 | (6.887 | 0.053 | 0.256 | 0.024 | 0.028 | 0.258) $\times 10^{-4}$ |
| 41.9 – 45.1 | (5.681 | 0.046 | 0.211 | 0.020 | 0.023 | 0.214) $\times 10^{-4}$ |
| 45.1 – 48.5 | (4.776 | 0.041 | 0.178 | 0.017 | 0.020 | 0.180) $\times 10^{-4}$ |
| 48.5 – 52.2 | (3.951 | 0.036 | 0.147 | 0.015 | 0.017 | 0.149) $\times 10^{-4}$ |
| 52.2 – 56.1 | (3.245 | 0.032 | 0.121 | 0.012 | 0.014 | 0.123) $\times 10^{-4}$ |

Table continued

TABLE SIII – (Continued).

| Rigidity [GV] | Φ | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|---------|-------------------------|------------------------|------------------------|-------------------------|--------------------------|
| 56.1 – 60.3 | (2.603 | 0.027 | 0.097 | 0.010 | 0.011 | 0.099) $\times 10^{-4}$ |
| 60.3 – 64.8 | (2.225 | 0.025 | 0.083 | 0.009 | 0.010 | 0.084) $\times 10^{-4}$ |
| 64.8 – 69.7 | (1.813 | 0.021 | 0.068 | 0.007 | 0.008 | 0.069) $\times 10^{-4}$ |
| 69.7 – 74.9 | (1.493 | 0.019 | 0.056 | 0.006 | 0.007 | 0.057) $\times 10^{-4}$ |
| 74.9 – 80.5 | (1.232 | 0.016 | 0.046 | 0.005 | 0.006 | 0.047) $\times 10^{-4}$ |
| 80.5 – 86.5 | (1.025 | 0.014 | 0.039 | 0.004 | 0.005 | 0.039) $\times 10^{-4}$ |
| 86.5 – 93.0 | (8.458 | 0.126 | 0.319 | 0.037 | 0.043 | 0.324) $\times 10^{-5}$ |
| 93.0 – 100 | (6.665 | 0.107 | 0.252 | 0.029 | 0.035 | 0.256) $\times 10^{-5}$ |
| 100 – 108 | (5.725 | 0.093 | 0.217 | 0.026 | 0.031 | 0.220) $\times 10^{-5}$ |
| 108 – 116 | (4.469 | 0.082 | 0.169 | 0.020 | 0.025 | 0.172) $\times 10^{-5}$ |
| 116 – 125 | (3.820 | 0.072 | 0.145 | 0.018 | 0.022 | 0.148) $\times 10^{-5}$ |
| 125 – 135 | (3.059 | 0.061 | 0.116 | 0.014 | 0.018 | 0.118) $\times 10^{-5}$ |
| 135 – 147 | (2.348 | 0.049 | 0.089 | 0.011 | 0.014 | 0.091) $\times 10^{-5}$ |
| 147 – 160 | (1.934 | 0.042 | 0.074 | 0.010 | 0.012 | 0.075) $\times 10^{-5}$ |
| 160 – 175 | (1.566 | 0.035 | 0.060 | 0.008 | 0.011 | 0.061) $\times 10^{-5}$ |
| 175 – 192 | (1.199 | 0.029 | 0.046 | 0.006 | 0.009 | 0.047) $\times 10^{-5}$ |
| 192 – 211 | (9.191 | 0.241 | 0.353 | 0.052 | 0.071 | 0.363) $\times 10^{-6}$ |
| 211 – 233 | (6.880 | 0.194 | 0.265 | 0.042 | 0.057 | 0.274) $\times 10^{-6}$ |
| 233 – 259 | (5.595 | 0.161 | 0.216 | 0.037 | 0.050 | 0.225) $\times 10^{-6}$ |
| 259 – 291 | (3.907 | 0.121 | 0.151 | 0.028 | 0.038 | 0.159) $\times 10^{-6}$ |
| 291 – 330 | (2.757 | 0.092 | 0.107 | 0.022 | 0.030 | 0.114) $\times 10^{-6}$ |
| 330 – 379 | (1.960 | 0.070 | 0.077 | 0.018 | 0.024 | 0.082) $\times 10^{-6}$ |
| 379 – 441 | (1.387 | 0.052 | 0.055 | 0.015 | 0.020 | 0.060) $\times 10^{-6}$ |
| 441 – 525 | (8.397 | 0.348 | 0.333 | 0.110 | 0.143 | 0.379) $\times 10^{-7}$ |
| 525 – 660 | (5.295 | 0.219 | 0.213 | 0.089 | 0.112 | 0.256) $\times 10^{-7}$ |
| 660 – 860 | (2.732 | 0.129 | 0.112 | 0.061 | 0.077 | 0.149) $\times 10^{-7}$ |
| 860 – 1200 | (1.146 | 0.064 | 0.048 | 0.036 | 0.046 | 0.076) $\times 10^{-7}$ |
| 1200 – 3000 | (1.999 | 0.293 | 0.105 | 0.036 | 0.115 | 0.160) $\times 10^{-8}$ |

TABLE SIV: The neon to magnesium flux ratio Ne/Mg as a function of rigidity including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The statistical errors are the sum in quadrature of the ratios of neon and magnesium flux statistical errors to the corresponding flux values, multiplied by the Ne/Mg flux ratio. The systematic errors from the background subtraction, the trigger, and the event reconstruction and selection are likewise added in quadrature. The correlations in the systematic errors from the uncertainty in nuclear interaction cross sections, the unfolding and the absolute rigidity scale between the neon and magnesium fluxes have been taken into account in calculating the corresponding systematic errors of the Ne/Mg flux ratio. The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic uncertainty.

| Rigidity [GV] | Ne/Mg | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 2.15 – 2.40 | 0.7697 | 0.0056 | 0.0236 | 0.0148 | 0.0000 | 0.0279 |
| 2.40 – 2.67 | 0.7834 | 0.0052 | 0.0238 | 0.0097 | 0.0000 | 0.0257 |
| 2.67 – 2.97 | 0.8006 | 0.0049 | 0.0241 | 0.0079 | 0.0000 | 0.0254 |
| 2.97 – 3.29 | 0.8209 | 0.0048 | 0.0246 | 0.0072 | 0.0000 | 0.0256 |
| 3.29 – 3.64 | 0.8249 | 0.0046 | 0.0246 | 0.0064 | 0.0000 | 0.0255 |
| 3.64 – 4.02 | 0.8303 | 0.0045 | 0.0247 | 0.0058 | 0.0000 | 0.0254 |
| 4.02 – 4.43 | 0.8276 | 0.0044 | 0.0246 | 0.0051 | 0.0000 | 0.0251 |
| 4.43 – 4.88 | 0.8372 | 0.0042 | 0.0249 | 0.0046 | 0.0000 | 0.0253 |
| 4.88 – 5.37 | 0.8292 | 0.0040 | 0.0246 | 0.0041 | 0.0000 | 0.0250 |
| 5.37 – 5.90 | 0.8297 | 0.0040 | 0.0247 | 0.0037 | 0.0000 | 0.0249 |
| 5.90 – 6.47 | 0.8436 | 0.0040 | 0.0251 | 0.0034 | 0.0000 | 0.0253 |
| 6.47 – 7.09 | 0.8426 | 0.0040 | 0.0251 | 0.0030 | 0.0000 | 0.0252 |
| 7.09 – 7.76 | 0.8342 | 0.0039 | 0.0248 | 0.0028 | 0.0000 | 0.0250 |
| 7.76 – 8.48 | 0.8408 | 0.0040 | 0.0250 | 0.0026 | 0.0000 | 0.0252 |
| 8.48 – 9.26 | 0.8509 | 0.0041 | 0.0253 | 0.0024 | 0.0000 | 0.0255 |
| 9.26 – 10.1 | 0.8405 | 0.0042 | 0.0250 | 0.0023 | 0.0000 | 0.0251 |
| 10.1 – 11.0 | 0.8381 | 0.0043 | 0.0250 | 0.0022 | 0.0000 | 0.0251 |
| 11.0 – 12.0 | 0.8465 | 0.0045 | 0.0252 | 0.0021 | 0.0000 | 0.0253 |
| 12.0 – 13.0 | 0.8357 | 0.0049 | 0.0249 | 0.0021 | 0.0000 | 0.0250 |
| 13.0 – 14.1 | 0.8391 | 0.0051 | 0.0250 | 0.0021 | 0.0000 | 0.0251 |
| 14.1 – 15.3 | 0.8301 | 0.0052 | 0.0248 | 0.0021 | 0.0000 | 0.0249 |
| 15.3 – 16.6 | 0.8243 | 0.0054 | 0.0246 | 0.0021 | 0.0000 | 0.0247 |
| 16.6 – 18.0 | 0.8345 | 0.0057 | 0.0249 | 0.0022 | 0.0000 | 0.0250 |
| 18.0 – 19.5 | 0.8341 | 0.0059 | 0.0249 | 0.0022 | 0.0000 | 0.0250 |
| 19.5 – 21.1 | 0.8306 | 0.0060 | 0.0249 | 0.0023 | 0.0000 | 0.0250 |
| 21.1 – 22.8 | 0.8387 | 0.0062 | 0.0251 | 0.0024 | 0.0000 | 0.0252 |
| 22.8 – 24.7 | 0.8468 | 0.0063 | 0.0254 | 0.0026 | 0.0000 | 0.0255 |
| 24.7 – 26.7 | 0.8396 | 0.0065 | 0.0252 | 0.0027 | 0.0000 | 0.0253 |
| 26.7 – 28.8 | 0.8426 | 0.0067 | 0.0253 | 0.0028 | 0.0000 | 0.0255 |
| 28.8 – 31.1 | 0.8216 | 0.0068 | 0.0247 | 0.0029 | 0.0000 | 0.0249 |
| 31.1 – 33.5 | 0.8238 | 0.0072 | 0.0248 | 0.0030 | 0.0000 | 0.0250 |

Table continued

TABLE SIV – (Continued).

| Rigidity [GV] | Ne/Mg | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 33.5 – 36.1 | 0.8323 | 0.0076 | 0.0251 | 0.0032 | 0.0000 | 0.0253 |
| 36.1 – 38.9 | 0.8225 | 0.0080 | 0.0249 | 0.0033 | 0.0000 | 0.0251 |
| 38.9 – 41.9 | 0.8506 | 0.0088 | 0.0258 | 0.0036 | 0.0000 | 0.0260 |
| 41.9 – 45.1 | 0.8303 | 0.0091 | 0.0252 | 0.0036 | 0.0000 | 0.0255 |
| 45.1 – 48.5 | 0.8362 | 0.0098 | 0.0254 | 0.0038 | 0.0000 | 0.0257 |
| 48.5 – 52.2 | 0.8386 | 0.0104 | 0.0256 | 0.0039 | 0.0000 | 0.0259 |
| 52.2 – 56.1 | 0.8431 | 0.0112 | 0.0258 | 0.0041 | 0.0000 | 0.0261 |
| 56.1 – 60.3 | 0.8341 | 0.0118 | 0.0255 | 0.0041 | 0.0000 | 0.0259 |
| 60.3 – 64.8 | 0.8310 | 0.0125 | 0.0255 | 0.0042 | 0.0000 | 0.0259 |
| 64.8 – 69.7 | 0.8413 | 0.0134 | 0.0259 | 0.0044 | 0.0000 | 0.0263 |
| 69.7 – 74.9 | 0.8340 | 0.0142 | 0.0257 | 0.0044 | 0.0000 | 0.0261 |
| 74.9 – 80.5 | 0.8653 | 0.0157 | 0.0267 | 0.0047 | 0.0000 | 0.0272 |
| 80.5 – 86.5 | 0.8296 | 0.0160 | 0.0257 | 0.0046 | 0.0000 | 0.0261 |
| 86.5 – 93.0 | 0.8359 | 0.0171 | 0.0259 | 0.0046 | 0.0001 | 0.0264 |
| 93.0 – 100 | 0.8227 | 0.0179 | 0.0256 | 0.0046 | 0.0001 | 0.0260 |
| 100 – 108 | 0.8383 | 0.0190 | 0.0261 | 0.0047 | 0.0001 | 0.0265 |
| 108 – 116 | 0.8046 | 0.0202 | 0.0251 | 0.0045 | 0.0001 | 0.0255 |
| 116 – 125 | 0.8256 | 0.0214 | 0.0258 | 0.0046 | 0.0001 | 0.0262 |
| 125 – 135 | 0.8154 | 0.0223 | 0.0255 | 0.0046 | 0.0001 | 0.0259 |
| 135 – 147 | 0.8506 | 0.0236 | 0.0267 | 0.0047 | 0.0001 | 0.0271 |
| 147 – 160 | 0.8118 | 0.0247 | 0.0255 | 0.0045 | 0.0001 | 0.0259 |
| 160 – 175 | 0.8093 | 0.0261 | 0.0255 | 0.0045 | 0.0001 | 0.0259 |
| 175 – 192 | 0.8249 | 0.0282 | 0.0261 | 0.0047 | 0.0001 | 0.0265 |
| 192 – 211 | 0.8190 | 0.0298 | 0.0260 | 0.0047 | 0.0001 | 0.0264 |
| 211 – 233 | 0.8223 | 0.0317 | 0.0262 | 0.0049 | 0.0001 | 0.0266 |
| 233 – 259 | 0.8400 | 0.0341 | 0.0268 | 0.0053 | 0.0000 | 0.0273 |
| 259 – 291 | 0.8193 | 0.0355 | 0.0263 | 0.0056 | 0.0001 | 0.0269 |
| 291 – 330 | 0.8139 | 0.0368 | 0.0262 | 0.0062 | 0.0002 | 0.0269 |
| 330 – 379 | 0.8651 | 0.0420 | 0.0280 | 0.0075 | 0.0004 | 0.0290 |
| 379 – 441 | 0.8813 | 0.0469 | 0.0287 | 0.0090 | 0.0006 | 0.0301 |
| 441 – 525 | 0.8838 | 0.0497 | 0.0290 | 0.0109 | 0.0009 | 0.0310 |
| 525 – 660 | 0.7701 | 0.0441 | 0.0255 | 0.0121 | 0.0011 | 0.0283 |
| 660 – 860 | 0.8517 | 0.0572 | 0.0285 | 0.0179 | 0.0018 | 0.0337 |
| 860 – 1200 | 0.8573 | 0.0634 | 0.0292 | 0.0250 | 0.0022 | 0.0385 |
| 1200 – 3000 | 1.1038 | 0.1932 | 0.0512 | 0.0202 | 0.0118 | 0.0563 |

TABLE SV: The silicon to magnesium flux ratio Si/Mg as a function of rigidity including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The statistical errors are the sum in quadrature of the ratios of silicon and magnesium flux statistical errors to the corresponding flux values, multiplied by the Si/Mg flux ratio. The systematic errors from the background subtraction, the trigger, and the event reconstruction and selection are likewise added in quadrature. The correlations in the systematic errors from the uncertainty in nuclear interaction cross sections, the unfolding and the absolute rigidity scale between the silicon and magnesium fluxes have been taken into account in calculating the corresponding systematic errors of the Si/Mg flux ratio. The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic uncertainty.

| Rigidity [GV] | Si/Mg | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 2.15 – 2.40 | 0.7052 | 0.0053 | 0.0226 | 0.0298 | 0.0001 | 0.0374 |
| 2.40 – 2.67 | 0.7166 | 0.0049 | 0.0226 | 0.0141 | 0.0001 | 0.0267 |
| 2.67 – 2.97 | 0.7325 | 0.0046 | 0.0229 | 0.0087 | 0.0000 | 0.0245 |
| 2.97 – 3.29 | 0.7455 | 0.0045 | 0.0231 | 0.0075 | 0.0000 | 0.0243 |
| 3.29 – 3.64 | 0.7455 | 0.0042 | 0.0230 | 0.0066 | 0.0000 | 0.0240 |
| 3.64 – 4.02 | 0.7462 | 0.0041 | 0.0230 | 0.0058 | 0.0000 | 0.0237 |
| 4.02 – 4.43 | 0.7418 | 0.0040 | 0.0228 | 0.0051 | 0.0000 | 0.0234 |
| 4.43 – 4.88 | 0.7494 | 0.0038 | 0.0230 | 0.0046 | 0.0000 | 0.0235 |
| 4.88 – 5.37 | 0.7387 | 0.0036 | 0.0227 | 0.0041 | 0.0000 | 0.0231 |
| 5.37 – 5.90 | 0.7352 | 0.0036 | 0.0226 | 0.0036 | 0.0000 | 0.0229 |
| 5.90 – 6.47 | 0.7539 | 0.0037 | 0.0232 | 0.0034 | 0.0000 | 0.0235 |
| 6.47 – 7.09 | 0.7534 | 0.0036 | 0.0232 | 0.0031 | 0.0000 | 0.0234 |
| 7.09 – 7.76 | 0.7643 | 0.0037 | 0.0236 | 0.0029 | 0.0000 | 0.0238 |
| 7.76 – 8.48 | 0.7548 | 0.0036 | 0.0233 | 0.0027 | 0.0000 | 0.0235 |
| 8.48 – 9.26 | 0.7662 | 0.0037 | 0.0237 | 0.0026 | 0.0000 | 0.0239 |
| 9.26 – 10.1 | 0.7711 | 0.0039 | 0.0239 | 0.0025 | 0.0000 | 0.0240 |
| 10.1 – 11.0 | 0.7739 | 0.0041 | 0.0240 | 0.0025 | 0.0000 | 0.0241 |
| 11.0 – 12.0 | 0.7797 | 0.0042 | 0.0242 | 0.0024 | 0.0000 | 0.0243 |
| 12.0 – 13.0 | 0.7867 | 0.0046 | 0.0244 | 0.0024 | 0.0000 | 0.0245 |
| 13.0 – 14.1 | 0.7928 | 0.0048 | 0.0246 | 0.0024 | 0.0000 | 0.0247 |
| 14.1 – 15.3 | 0.7841 | 0.0050 | 0.0244 | 0.0023 | 0.0000 | 0.0245 |
| 15.3 – 16.6 | 0.7884 | 0.0052 | 0.0245 | 0.0023 | 0.0000 | 0.0246 |
| 16.6 – 18.0 | 0.7912 | 0.0054 | 0.0246 | 0.0024 | 0.0000 | 0.0247 |
| 18.0 – 19.5 | 0.7903 | 0.0056 | 0.0246 | 0.0024 | 0.0000 | 0.0247 |
| 19.5 – 21.1 | 0.8038 | 0.0059 | 0.0250 | 0.0025 | 0.0000 | 0.0251 |
| 21.1 – 22.8 | 0.8032 | 0.0060 | 0.0250 | 0.0025 | 0.0000 | 0.0251 |
| 22.8 – 24.7 | 0.8047 | 0.0060 | 0.0251 | 0.0026 | 0.0001 | 0.0252 |
| 24.7 – 26.7 | 0.8148 | 0.0063 | 0.0254 | 0.0027 | 0.0001 | 0.0256 |
| 26.7 – 28.8 | 0.8217 | 0.0066 | 0.0257 | 0.0028 | 0.0001 | 0.0258 |
| 28.8 – 31.1 | 0.8219 | 0.0067 | 0.0257 | 0.0029 | 0.0001 | 0.0259 |
| 31.1 – 33.5 | 0.8268 | 0.0072 | 0.0259 | 0.0030 | 0.0001 | 0.0261 |

Table continued

TABLE SV – (Continued).

| Rigidity [GV] | Si/Mg | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 33.5 – 36.1 | 0.8267 | 0.0075 | 0.0260 | 0.0031 | 0.0001 | 0.0262 |
| 36.1 – 38.9 | 0.8411 | 0.0081 | 0.0265 | 0.0032 | 0.0001 | 0.0267 |
| 38.9 – 41.9 | 0.8488 | 0.0088 | 0.0268 | 0.0033 | 0.0001 | 0.0270 |
| 41.9 – 45.1 | 0.8323 | 0.0091 | 0.0264 | 0.0034 | 0.0001 | 0.0266 |
| 45.1 – 48.5 | 0.8630 | 0.0101 | 0.0274 | 0.0036 | 0.0001 | 0.0277 |
| 48.5 – 52.2 | 0.8652 | 0.0107 | 0.0276 | 0.0037 | 0.0001 | 0.0278 |
| 52.2 – 56.1 | 0.8648 | 0.0114 | 0.0277 | 0.0038 | 0.0001 | 0.0279 |
| 56.1 – 60.3 | 0.8408 | 0.0119 | 0.0270 | 0.0038 | 0.0001 | 0.0273 |
| 60.3 – 64.8 | 0.8786 | 0.0131 | 0.0283 | 0.0040 | 0.0002 | 0.0286 |
| 64.8 – 69.7 | 0.8735 | 0.0138 | 0.0283 | 0.0041 | 0.0002 | 0.0285 |
| 69.7 – 74.9 | 0.8709 | 0.0147 | 0.0283 | 0.0041 | 0.0002 | 0.0286 |
| 74.9 – 80.5 | 0.8997 | 0.0162 | 0.0293 | 0.0043 | 0.0002 | 0.0296 |
| 80.5 – 86.5 | 0.8861 | 0.0169 | 0.0289 | 0.0043 | 0.0002 | 0.0293 |
| 86.5 – 93.0 | 0.8972 | 0.0181 | 0.0294 | 0.0044 | 0.0002 | 0.0297 |
| 93.0 – 100 | 0.8564 | 0.0186 | 0.0281 | 0.0042 | 0.0002 | 0.0284 |
| 100 – 108 | 0.9199 | 0.0205 | 0.0303 | 0.0046 | 0.0002 | 0.0306 |
| 108 – 116 | 0.8597 | 0.0213 | 0.0284 | 0.0043 | 0.0002 | 0.0287 |
| 116 – 125 | 0.8960 | 0.0229 | 0.0296 | 0.0045 | 0.0001 | 0.0300 |
| 125 – 135 | 0.8829 | 0.0238 | 0.0293 | 0.0044 | 0.0001 | 0.0296 |
| 135 – 147 | 0.8583 | 0.0239 | 0.0286 | 0.0043 | 0.0001 | 0.0289 |
| 147 – 160 | 0.8980 | 0.0268 | 0.0300 | 0.0045 | 0.0001 | 0.0303 |
| 160 – 175 | 0.9362 | 0.0292 | 0.0314 | 0.0048 | 0.0001 | 0.0318 |
| 175 – 192 | 0.9258 | 0.0309 | 0.0312 | 0.0049 | 0.0001 | 0.0316 |
| 192 – 211 | 0.8966 | 0.0321 | 0.0303 | 0.0050 | 0.0001 | 0.0307 |
| 211 – 233 | 0.8756 | 0.0335 | 0.0298 | 0.0051 | 0.0001 | 0.0302 |
| 233 – 259 | 0.9401 | 0.0373 | 0.0321 | 0.0059 | 0.0001 | 0.0327 |
| 259 – 291 | 0.9076 | 0.0385 | 0.0312 | 0.0063 | 0.0001 | 0.0318 |
| 291 – 330 | 0.8492 | 0.0383 | 0.0294 | 0.0066 | 0.0001 | 0.0301 |
| 330 – 379 | 0.8994 | 0.0435 | 0.0313 | 0.0081 | 0.0000 | 0.0324 |
| 379 – 441 | 0.9798 | 0.0512 | 0.0344 | 0.0104 | 0.0000 | 0.0360 |
| 441 – 525 | 0.8954 | 0.0506 | 0.0318 | 0.0116 | 0.0000 | 0.0338 |
| 525 – 660 | 0.8705 | 0.0486 | 0.0313 | 0.0145 | 0.0001 | 0.0345 |
| 660 – 860 | 0.9618 | 0.0631 | 0.0351 | 0.0214 | 0.0001 | 0.0411 |
| 860 – 1200 | 0.8279 | 0.0624 | 0.0308 | 0.0258 | 0.0002 | 0.0402 |
| 1200 – 3000 | 0.7906 | 0.1531 | 0.0398 | 0.0149 | 0.0020 | 0.0426 |

TABLE SVI: The neon to oxygen flux ratio Ne/O as a function of rigidity including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The statistical errors are the sum in quadrature of the ratios of neon and oxygen flux statistical errors to the corresponding flux values, multiplied by the Ne/O flux ratio. The systematic errors from the background subtraction, the trigger, and the event reconstruction and selection are likewise added in quadrature. The correlations in the systematic errors from the uncertainty in nuclear interaction cross sections, the unfolding and the absolute rigidity scale between the neon and oxygen fluxes have been taken into account in calculating the corresponding systematic errors of the Ne/O flux ratio. The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic uncertainty.

| Rigidity [GV] | Ne/O | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 2.15 – 2.40 | 0.1535 | 0.0009 | 0.0046 | 0.0029 | 0.0000 | 0.0055 |
| 2.40 – 2.67 | 0.1544 | 0.0008 | 0.0045 | 0.0018 | 0.0000 | 0.0048 |
| 2.67 – 2.97 | 0.1543 | 0.0008 | 0.0043 | 0.0014 | 0.0000 | 0.0046 |
| 2.97 – 3.29 | 0.1569 | 0.0007 | 0.0043 | 0.0012 | 0.0000 | 0.0045 |
| 3.29 – 3.64 | 0.1603 | 0.0007 | 0.0044 | 0.0011 | 0.0000 | 0.0045 |
| 3.64 – 4.02 | 0.1615 | 0.0007 | 0.0044 | 0.0010 | 0.0000 | 0.0045 |
| 4.02 – 4.43 | 0.1626 | 0.0007 | 0.0044 | 0.0009 | 0.0000 | 0.0044 |
| 4.43 – 4.88 | 0.1658 | 0.0007 | 0.0044 | 0.0008 | 0.0000 | 0.0045 |
| 4.88 – 5.37 | 0.1665 | 0.0006 | 0.0044 | 0.0007 | 0.0000 | 0.0045 |
| 5.37 – 5.90 | 0.1678 | 0.0006 | 0.0045 | 0.0006 | 0.0000 | 0.0045 |
| 5.90 – 6.47 | 0.1700 | 0.0006 | 0.0045 | 0.0006 | 0.0000 | 0.0045 |
| 6.47 – 7.09 | 0.1708 | 0.0006 | 0.0045 | 0.0005 | 0.0000 | 0.0046 |
| 7.09 – 7.76 | 0.1704 | 0.0006 | 0.0045 | 0.0005 | 0.0000 | 0.0046 |
| 7.76 – 8.48 | 0.1723 | 0.0006 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 8.48 – 9.26 | 0.1746 | 0.0007 | 0.0047 | 0.0004 | 0.0000 | 0.0047 |
| 9.26 – 10.1 | 0.1727 | 0.0007 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 10.1 – 11.0 | 0.1738 | 0.0007 | 0.0046 | 0.0004 | 0.0000 | 0.0047 |
| 11.0 – 12.0 | 0.1738 | 0.0007 | 0.0046 | 0.0004 | 0.0000 | 0.0047 |
| 12.0 – 13.0 | 0.1712 | 0.0008 | 0.0046 | 0.0003 | 0.0000 | 0.0046 |
| 13.0 – 14.1 | 0.1723 | 0.0008 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 14.1 – 15.3 | 0.1722 | 0.0009 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 15.3 – 16.6 | 0.1700 | 0.0009 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 16.6 – 18.0 | 0.1716 | 0.0009 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 18.0 – 19.5 | 0.1716 | 0.0010 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 19.5 – 21.1 | 0.1694 | 0.0010 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 21.1 – 22.8 | 0.1702 | 0.0010 | 0.0046 | 0.0004 | 0.0000 | 0.0046 |
| 22.8 – 24.7 | 0.1720 | 0.0010 | 0.0047 | 0.0005 | 0.0000 | 0.0047 |
| 24.7 – 26.7 | 0.1707 | 0.0010 | 0.0046 | 0.0005 | 0.0000 | 0.0047 |
| 26.7 – 28.8 | 0.1716 | 0.0011 | 0.0047 | 0.0005 | 0.0000 | 0.0047 |
| 28.8 – 31.1 | 0.1673 | 0.0011 | 0.0046 | 0.0005 | 0.0000 | 0.0046 |
| 31.1 – 33.5 | 0.1676 | 0.0012 | 0.0046 | 0.0006 | 0.0000 | 0.0046 |
| 33.5 – 36.1 | 0.1697 | 0.0012 | 0.0047 | 0.0006 | 0.0000 | 0.0047 |

Table continued

TABLE SVI – (Continued).

| Rigidity [GV] | Ne/O | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 36.1 – 38.9 | 0.1663 | 0.0013 | 0.0046 | 0.0006 | 0.0000 | 0.0046 |
| 38.9 – 41.9 | 0.1703 | 0.0014 | 0.0047 | 0.0007 | 0.0000 | 0.0048 |
| 41.9 – 45.1 | 0.1690 | 0.0015 | 0.0047 | 0.0007 | 0.0000 | 0.0048 |
| 45.1 – 48.5 | 0.1668 | 0.0016 | 0.0047 | 0.0007 | 0.0000 | 0.0047 |
| 48.5 – 52.2 | 0.1672 | 0.0016 | 0.0047 | 0.0007 | 0.0000 | 0.0048 |
| 52.2 – 56.1 | 0.1677 | 0.0018 | 0.0047 | 0.0008 | 0.0000 | 0.0048 |
| 56.1 – 60.3 | 0.1671 | 0.0019 | 0.0047 | 0.0008 | 0.0000 | 0.0048 |
| 60.3 – 64.8 | 0.1643 | 0.0020 | 0.0047 | 0.0008 | 0.0000 | 0.0047 |
| 64.8 – 69.7 | 0.1660 | 0.0021 | 0.0048 | 0.0008 | 0.0000 | 0.0048 |
| 69.7 – 74.9 | 0.1663 | 0.0023 | 0.0048 | 0.0009 | 0.0000 | 0.0049 |
| 74.9 – 80.5 | 0.1666 | 0.0024 | 0.0048 | 0.0009 | 0.0000 | 0.0049 |
| 80.5 – 86.5 | 0.1635 | 0.0025 | 0.0048 | 0.0009 | 0.0000 | 0.0048 |
| 86.5 – 93.0 | 0.1637 | 0.0027 | 0.0048 | 0.0009 | 0.0000 | 0.0049 |
| 93.0 – 100 | 0.1627 | 0.0028 | 0.0048 | 0.0009 | 0.0001 | 0.0049 |
| 100 – 108 | 0.1614 | 0.0029 | 0.0048 | 0.0009 | 0.0001 | 0.0049 |
| 108 – 116 | 0.1575 | 0.0032 | 0.0047 | 0.0009 | 0.0001 | 0.0048 |
| 116 – 125 | 0.1613 | 0.0033 | 0.0049 | 0.0009 | 0.0001 | 0.0049 |
| 125 – 135 | 0.1598 | 0.0035 | 0.0048 | 0.0009 | 0.0001 | 0.0049 |
| 135 – 147 | 0.1641 | 0.0036 | 0.0050 | 0.0010 | 0.0001 | 0.0051 |
| 147 – 160 | 0.1571 | 0.0038 | 0.0048 | 0.0009 | 0.0001 | 0.0049 |
| 160 – 175 | 0.1532 | 0.0039 | 0.0048 | 0.0009 | 0.0001 | 0.0049 |
| 175 – 192 | 0.1537 | 0.0042 | 0.0048 | 0.0010 | 0.0001 | 0.0049 |
| 192 – 211 | 0.1542 | 0.0045 | 0.0049 | 0.0010 | 0.0001 | 0.0050 |
| 211 – 233 | 0.1552 | 0.0047 | 0.0050 | 0.0011 | 0.0000 | 0.0051 |
| 233 – 259 | 0.1588 | 0.0051 | 0.0052 | 0.0012 | 0.0000 | 0.0053 |
| 259 – 291 | 0.1485 | 0.0051 | 0.0049 | 0.0012 | 0.0000 | 0.0050 |
| 291 – 330 | 0.1548 | 0.0056 | 0.0052 | 0.0014 | 0.0000 | 0.0053 |
| 330 – 379 | 0.1564 | 0.0059 | 0.0053 | 0.0016 | 0.0001 | 0.0055 |
| 379 – 441 | 0.1534 | 0.0064 | 0.0053 | 0.0018 | 0.0002 | 0.0056 |
| 441 – 525 | 0.1604 | 0.0070 | 0.0057 | 0.0023 | 0.0003 | 0.0061 |
| 525 – 660 | 0.1529 | 0.0070 | 0.0055 | 0.0028 | 0.0005 | 0.0062 |
| 660 – 860 | 0.1476 | 0.0078 | 0.0055 | 0.0036 | 0.0006 | 0.0066 |
| 860 – 1200 | 0.1542 | 0.0089 | 0.0060 | 0.0053 | 0.0007 | 0.0080 |
| 1200 – 3000 | 0.1798 | 0.0232 | 0.0093 | 0.0054 | 0.0003 | 0.0107 |

TABLE SVII: The magnesium to oxygen flux ratio Mg/O as a function of rigidity including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The statistical errors are the sum in quadrature of the ratios of magnesium and oxygen flux statistical errors to the corresponding flux values, multiplied by the Mg/O flux ratio. The systematic errors from the background subtraction, the trigger, and the event reconstruction and selection are likewise added in quadrature. The correlations in the systematic errors from the uncertainty in nuclear interaction cross sections, the unfolding and the absolute rigidity scale between the magnesium and oxygen fluxes have been taken into account in calculating the corresponding systematic errors of the Mg/O flux ratio. The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic uncertainty.

| Rigidity [GV] | Mg/O | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 2.15 – 2.40 | 0.1994 | 0.0010 | 0.0061 | 0.0025 | 0.0000 | 0.0066 |
| 2.40 – 2.67 | 0.1971 | 0.0009 | 0.0058 | 0.0022 | 0.0000 | 0.0062 |
| 2.67 – 2.97 | 0.1928 | 0.0008 | 0.0055 | 0.0019 | 0.0000 | 0.0058 |
| 2.97 – 3.29 | 0.1912 | 0.0008 | 0.0054 | 0.0016 | 0.0000 | 0.0056 |
| 3.29 – 3.64 | 0.1943 | 0.0008 | 0.0054 | 0.0014 | 0.0000 | 0.0056 |
| 3.64 – 4.02 | 0.1945 | 0.0008 | 0.0053 | 0.0013 | 0.0000 | 0.0055 |
| 4.02 – 4.43 | 0.1965 | 0.0008 | 0.0053 | 0.0011 | 0.0000 | 0.0055 |
| 4.43 – 4.88 | 0.1981 | 0.0007 | 0.0054 | 0.0010 | 0.0000 | 0.0055 |
| 4.88 – 5.37 | 0.2008 | 0.0007 | 0.0054 | 0.0009 | 0.0000 | 0.0055 |
| 5.37 – 5.90 | 0.2023 | 0.0007 | 0.0055 | 0.0008 | 0.0000 | 0.0055 |
| 5.90 – 6.47 | 0.2015 | 0.0007 | 0.0054 | 0.0007 | 0.0000 | 0.0055 |
| 6.47 – 7.09 | 0.2027 | 0.0007 | 0.0055 | 0.0007 | 0.0000 | 0.0055 |
| 7.09 – 7.76 | 0.2043 | 0.0007 | 0.0055 | 0.0006 | 0.0000 | 0.0056 |
| 7.76 – 8.48 | 0.2049 | 0.0007 | 0.0055 | 0.0006 | 0.0000 | 0.0056 |
| 8.48 – 9.26 | 0.2052 | 0.0007 | 0.0056 | 0.0006 | 0.0000 | 0.0056 |
| 9.26 – 10.1 | 0.2054 | 0.0007 | 0.0056 | 0.0005 | 0.0000 | 0.0056 |
| 10.1 – 11.0 | 0.2073 | 0.0008 | 0.0056 | 0.0005 | 0.0000 | 0.0057 |
| 11.0 – 12.0 | 0.2054 | 0.0008 | 0.0056 | 0.0005 | 0.0000 | 0.0056 |
| 12.0 – 13.0 | 0.2049 | 0.0009 | 0.0056 | 0.0005 | 0.0000 | 0.0056 |
| 13.0 – 14.1 | 0.2054 | 0.0009 | 0.0056 | 0.0005 | 0.0000 | 0.0056 |
| 14.1 – 15.3 | 0.2075 | 0.0009 | 0.0057 | 0.0005 | 0.0000 | 0.0057 |
| 15.3 – 16.6 | 0.2062 | 0.0010 | 0.0056 | 0.0005 | 0.0000 | 0.0057 |
| 16.6 – 18.0 | 0.2056 | 0.0010 | 0.0056 | 0.0005 | 0.0000 | 0.0056 |
| 18.0 – 19.5 | 0.2057 | 0.0011 | 0.0056 | 0.0005 | 0.0000 | 0.0057 |
| 19.5 – 21.1 | 0.2039 | 0.0011 | 0.0056 | 0.0006 | 0.0000 | 0.0056 |
| 21.1 – 22.8 | 0.2030 | 0.0011 | 0.0056 | 0.0006 | 0.0000 | 0.0056 |
| 22.8 – 24.7 | 0.2031 | 0.0011 | 0.0056 | 0.0006 | 0.0000 | 0.0056 |
| 24.7 – 26.7 | 0.2033 | 0.0011 | 0.0056 | 0.0006 | 0.0000 | 0.0056 |
| 26.7 – 28.8 | 0.2037 | 0.0012 | 0.0056 | 0.0007 | 0.0000 | 0.0057 |
| 28.8 – 31.1 | 0.2036 | 0.0012 | 0.0057 | 0.0007 | 0.0000 | 0.0057 |
| 31.1 – 33.5 | 0.2034 | 0.0013 | 0.0057 | 0.0007 | 0.0000 | 0.0057 |

Table continued

TABLE SVII – (Continued).

| Rigidity [GV] | Mg/O | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 33.5 – 36.1 | 0.2038 | 0.0013 | 0.0057 | 0.0008 | 0.0000 | 0.0058 |
| 36.1 – 38.9 | 0.2022 | 0.0014 | 0.0057 | 0.0008 | 0.0000 | 0.0057 |
| 38.9 – 41.9 | 0.2002 | 0.0015 | 0.0056 | 0.0008 | 0.0000 | 0.0057 |
| 41.9 – 45.1 | 0.2036 | 0.0016 | 0.0058 | 0.0008 | 0.0000 | 0.0058 |
| 45.1 – 48.5 | 0.1995 | 0.0017 | 0.0057 | 0.0009 | 0.0000 | 0.0057 |
| 48.5 – 52.2 | 0.1994 | 0.0018 | 0.0057 | 0.0009 | 0.0000 | 0.0058 |
| 52.2 – 56.1 | 0.1989 | 0.0019 | 0.0057 | 0.0009 | 0.0000 | 0.0058 |
| 56.1 – 60.3 | 0.2003 | 0.0021 | 0.0058 | 0.0009 | 0.0000 | 0.0059 |
| 60.3 – 64.8 | 0.1976 | 0.0022 | 0.0058 | 0.0010 | 0.0000 | 0.0058 |
| 64.8 – 69.7 | 0.1974 | 0.0023 | 0.0058 | 0.0010 | 0.0000 | 0.0059 |
| 69.7 – 74.9 | 0.1994 | 0.0025 | 0.0059 | 0.0010 | 0.0000 | 0.0060 |
| 74.9 – 80.5 | 0.1926 | 0.0026 | 0.0057 | 0.0010 | 0.0000 | 0.0058 |
| 80.5 – 86.5 | 0.1971 | 0.0028 | 0.0059 | 0.0010 | 0.0000 | 0.0060 |
| 86.5 – 93.0 | 0.1959 | 0.0029 | 0.0059 | 0.0010 | 0.0000 | 0.0060 |
| 93.0 – 100 | 0.1978 | 0.0031 | 0.0060 | 0.0011 | 0.0000 | 0.0061 |
| 100 – 108 | 0.1925 | 0.0032 | 0.0059 | 0.0010 | 0.0001 | 0.0060 |
| 108 – 116 | 0.1958 | 0.0035 | 0.0060 | 0.0011 | 0.0001 | 0.0061 |
| 116 – 125 | 0.1953 | 0.0037 | 0.0060 | 0.0011 | 0.0001 | 0.0061 |
| 125 – 135 | 0.1959 | 0.0039 | 0.0061 | 0.0011 | 0.0001 | 0.0062 |
| 135 – 147 | 0.1929 | 0.0039 | 0.0061 | 0.0011 | 0.0001 | 0.0061 |
| 147 – 160 | 0.1935 | 0.0042 | 0.0061 | 0.0011 | 0.0001 | 0.0062 |
| 160 – 175 | 0.1894 | 0.0044 | 0.0061 | 0.0011 | 0.0001 | 0.0062 |
| 175 – 192 | 0.1863 | 0.0046 | 0.0060 | 0.0011 | 0.0001 | 0.0061 |
| 192 – 211 | 0.1883 | 0.0049 | 0.0061 | 0.0012 | 0.0001 | 0.0063 |
| 211 – 233 | 0.1887 | 0.0053 | 0.0062 | 0.0012 | 0.0000 | 0.0064 |
| 233 – 259 | 0.1891 | 0.0056 | 0.0063 | 0.0013 | 0.0000 | 0.0065 |
| 259 – 291 | 0.1813 | 0.0056 | 0.0061 | 0.0014 | 0.0000 | 0.0063 |
| 291 – 330 | 0.1902 | 0.0062 | 0.0065 | 0.0017 | 0.0000 | 0.0067 |
| 330 – 379 | 0.1808 | 0.0064 | 0.0063 | 0.0018 | 0.0000 | 0.0066 |
| 379 – 441 | 0.1740 | 0.0068 | 0.0062 | 0.0021 | 0.0001 | 0.0065 |
| 441 – 525 | 0.1815 | 0.0075 | 0.0066 | 0.0027 | 0.0002 | 0.0071 |
| 525 – 660 | 0.1985 | 0.0081 | 0.0074 | 0.0037 | 0.0003 | 0.0083 |
| 660 – 860 | 0.1732 | 0.0084 | 0.0067 | 0.0044 | 0.0003 | 0.0080 |
| 860 – 1200 | 0.1799 | 0.0097 | 0.0072 | 0.0063 | 0.0004 | 0.0096 |
| 1200 – 3000 | 0.1629 | 0.0218 | 0.0084 | 0.0049 | 0.0015 | 0.0098 |

TABLE SVIII: The silicon to oxygen flux ratio Si/O as a function of rigidity including errors due to statistics (stat.); contributions to the systematic error from the trigger, acceptance, and background (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The statistical errors are the sum in quadrature of the ratios of silicon and oxygen flux statistical errors to the corresponding flux values, multiplied by the Si/O flux ratio. The systematic errors from the background subtraction, the trigger, and the event reconstruction and selection are likewise added in quadrature. The correlations in the systematic errors from the uncertainty in nuclear interaction cross sections, the unfolding and the absolute rigidity scale between the silicon and oxygen fluxes have been taken into account in calculating the corresponding systematic errors of the Si/O flux ratio. The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic uncertainty.

| Rigidity [GV] | Si/O | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 2.15 – 2.40 | 0.1406 | 0.0009 | 0.0045 | 0.0060 | 0.0000 | 0.0075 |
| 2.40 – 2.67 | 0.1413 | 0.0008 | 0.0043 | 0.0028 | 0.0000 | 0.0052 |
| 2.67 – 2.97 | 0.1412 | 0.0007 | 0.0042 | 0.0016 | 0.0000 | 0.0045 |
| 2.97 – 3.29 | 0.1425 | 0.0007 | 0.0041 | 0.0014 | 0.0000 | 0.0044 |
| 3.29 – 3.64 | 0.1449 | 0.0007 | 0.0041 | 0.0012 | 0.0000 | 0.0043 |
| 3.64 – 4.02 | 0.1452 | 0.0007 | 0.0041 | 0.0011 | 0.0000 | 0.0042 |
| 4.02 – 4.43 | 0.1457 | 0.0006 | 0.0041 | 0.0009 | 0.0000 | 0.0042 |
| 4.43 – 4.88 | 0.1484 | 0.0006 | 0.0041 | 0.0008 | 0.0000 | 0.0042 |
| 4.88 – 5.37 | 0.1484 | 0.0006 | 0.0041 | 0.0007 | 0.0000 | 0.0042 |
| 5.37 – 5.90 | 0.1487 | 0.0006 | 0.0041 | 0.0007 | 0.0000 | 0.0042 |
| 5.90 – 6.47 | 0.1519 | 0.0006 | 0.0042 | 0.0006 | 0.0000 | 0.0043 |
| 6.47 – 7.09 | 0.1527 | 0.0006 | 0.0042 | 0.0006 | 0.0000 | 0.0043 |
| 7.09 – 7.76 | 0.1562 | 0.0006 | 0.0044 | 0.0006 | 0.0000 | 0.0044 |
| 7.76 – 8.48 | 0.1547 | 0.0006 | 0.0043 | 0.0005 | 0.0000 | 0.0043 |
| 8.48 – 9.26 | 0.1572 | 0.0006 | 0.0044 | 0.0005 | 0.0000 | 0.0044 |
| 9.26 – 10.1 | 0.1584 | 0.0006 | 0.0044 | 0.0005 | 0.0000 | 0.0045 |
| 10.1 – 11.0 | 0.1605 | 0.0007 | 0.0045 | 0.0005 | 0.0000 | 0.0045 |
| 11.0 – 12.0 | 0.1601 | 0.0007 | 0.0045 | 0.0005 | 0.0000 | 0.0045 |
| 12.0 – 13.0 | 0.1612 | 0.0008 | 0.0045 | 0.0005 | 0.0000 | 0.0046 |
| 13.0 – 14.1 | 0.1628 | 0.0008 | 0.0046 | 0.0005 | 0.0000 | 0.0046 |
| 14.1 – 15.3 | 0.1627 | 0.0008 | 0.0046 | 0.0005 | 0.0000 | 0.0046 |
| 15.3 – 16.6 | 0.1626 | 0.0009 | 0.0046 | 0.0005 | 0.0000 | 0.0046 |
| 16.6 – 18.0 | 0.1627 | 0.0009 | 0.0046 | 0.0005 | 0.0000 | 0.0046 |
| 18.0 – 19.5 | 0.1626 | 0.0009 | 0.0046 | 0.0005 | 0.0000 | 0.0046 |
| 19.5 – 21.1 | 0.1639 | 0.0010 | 0.0046 | 0.0005 | 0.0000 | 0.0047 |
| 21.1 – 22.8 | 0.1630 | 0.0010 | 0.0046 | 0.0005 | 0.0000 | 0.0047 |
| 22.8 – 24.7 | 0.1635 | 0.0010 | 0.0047 | 0.0005 | 0.0000 | 0.0047 |
| 24.7 – 26.7 | 0.1656 | 0.0010 | 0.0047 | 0.0005 | 0.0000 | 0.0048 |
| 26.7 – 28.8 | 0.1674 | 0.0011 | 0.0048 | 0.0005 | 0.0000 | 0.0048 |
| 28.8 – 31.1 | 0.1674 | 0.0011 | 0.0048 | 0.0005 | 0.0000 | 0.0048 |
| 31.1 – 33.5 | 0.1682 | 0.0012 | 0.0048 | 0.0006 | 0.0000 | 0.0049 |
| 33.5 – 36.1 | 0.1685 | 0.0012 | 0.0049 | 0.0006 | 0.0000 | 0.0049 |

Table continued

TABLE SVIII – (Continued).

| Rigidity [GV] | Si/O | $\sigma_{\text{stat.}}$ | $\sigma_{\text{acc.}}$ | $\sigma_{\text{unf.}}$ | σ_{scale} | $\sigma_{\text{syst.}}$ |
|---------------|--------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 36.1 – 38.9 | 0.1701 | 0.0013 | 0.0049 | 0.0006 | 0.0000 | 0.0050 |
| 38.9 – 41.9 | 0.1700 | 0.0014 | 0.0050 | 0.0006 | 0.0000 | 0.0050 |
| 41.9 – 45.1 | 0.1694 | 0.0015 | 0.0050 | 0.0006 | 0.0000 | 0.0050 |
| 45.1 – 48.5 | 0.1721 | 0.0016 | 0.0051 | 0.0007 | 0.0000 | 0.0051 |
| 48.5 – 52.2 | 0.1725 | 0.0017 | 0.0051 | 0.0007 | 0.0000 | 0.0052 |
| 52.2 – 56.1 | 0.1720 | 0.0018 | 0.0051 | 0.0007 | 0.0000 | 0.0052 |
| 56.1 – 60.3 | 0.1684 | 0.0019 | 0.0050 | 0.0007 | 0.0000 | 0.0051 |
| 60.3 – 64.8 | 0.1737 | 0.0020 | 0.0052 | 0.0008 | 0.0000 | 0.0053 |
| 64.8 – 69.7 | 0.1724 | 0.0022 | 0.0052 | 0.0008 | 0.0000 | 0.0053 |
| 69.7 – 74.9 | 0.1737 | 0.0023 | 0.0053 | 0.0008 | 0.0000 | 0.0054 |
| 74.9 – 80.5 | 0.1733 | 0.0025 | 0.0053 | 0.0008 | 0.0000 | 0.0054 |
| 80.5 – 86.5 | 0.1747 | 0.0026 | 0.0054 | 0.0008 | 0.0000 | 0.0055 |
| 86.5 – 93.0 | 0.1757 | 0.0028 | 0.0055 | 0.0009 | 0.0000 | 0.0055 |
| 93.0 – 100 | 0.1694 | 0.0029 | 0.0053 | 0.0008 | 0.0000 | 0.0054 |
| 100 – 108 | 0.1771 | 0.0031 | 0.0056 | 0.0009 | 0.0000 | 0.0057 |
| 108 – 116 | 0.1683 | 0.0033 | 0.0053 | 0.0009 | 0.0000 | 0.0054 |
| 116 – 125 | 0.1750 | 0.0035 | 0.0056 | 0.0009 | 0.0000 | 0.0057 |
| 125 – 135 | 0.1730 | 0.0037 | 0.0056 | 0.0009 | 0.0000 | 0.0057 |
| 135 – 147 | 0.1655 | 0.0037 | 0.0054 | 0.0009 | 0.0000 | 0.0055 |
| 147 – 160 | 0.1737 | 0.0041 | 0.0057 | 0.0010 | 0.0000 | 0.0058 |
| 160 – 175 | 0.1773 | 0.0043 | 0.0059 | 0.0010 | 0.0000 | 0.0060 |
| 175 – 192 | 0.1725 | 0.0045 | 0.0058 | 0.0010 | 0.0000 | 0.0059 |
| 192 – 211 | 0.1688 | 0.0047 | 0.0057 | 0.0011 | 0.0000 | 0.0058 |
| 211 – 233 | 0.1652 | 0.0050 | 0.0057 | 0.0011 | 0.0000 | 0.0058 |
| 233 – 259 | 0.1777 | 0.0055 | 0.0062 | 0.0013 | 0.0000 | 0.0063 |
| 259 – 291 | 0.1645 | 0.0055 | 0.0058 | 0.0013 | 0.0000 | 0.0059 |
| 291 – 330 | 0.1615 | 0.0058 | 0.0058 | 0.0015 | 0.0000 | 0.0059 |
| 330 – 379 | 0.1626 | 0.0061 | 0.0059 | 0.0017 | 0.0000 | 0.0061 |
| 379 – 441 | 0.1705 | 0.0068 | 0.0063 | 0.0021 | 0.0001 | 0.0066 |
| 441 – 525 | 0.1625 | 0.0072 | 0.0061 | 0.0024 | 0.0001 | 0.0066 |
| 525 – 660 | 0.1728 | 0.0076 | 0.0067 | 0.0033 | 0.0003 | 0.0075 |
| 660 – 860 | 0.1666 | 0.0084 | 0.0067 | 0.0042 | 0.0003 | 0.0079 |
| 860 – 1200 | 0.1489 | 0.0089 | 0.0062 | 0.0053 | 0.0003 | 0.0082 |
| 1200 – 3000 | 0.1288 | 0.0197 | 0.0072 | 0.0038 | 0.0008 | 0.0082 |

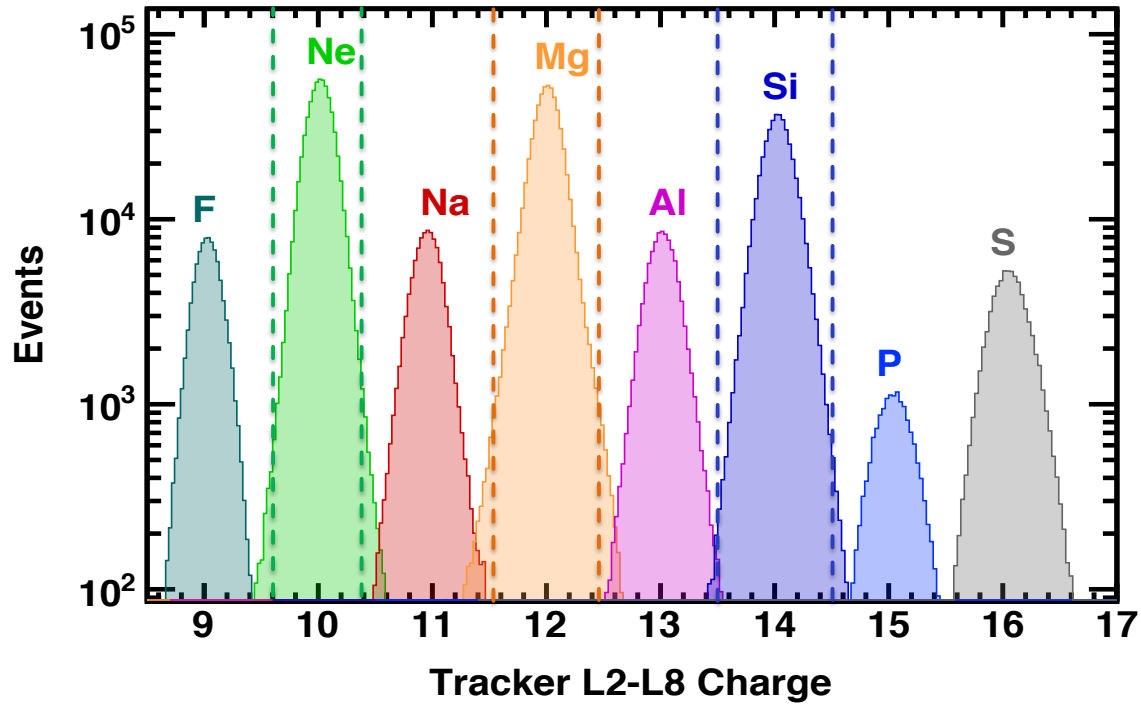


FIG. S1. Distribution of the charge measured with the inner tracker $L2-L8$ for samples from $Z = 9$ to $Z = 16$ selected by the combined charge measured with $L1$, the upper TOF, and the lower TOF over the rigidities above 4 GV. The colored vertical lines correspond to the charge selection in the inner tracker for neon (green), magnesium (orange) and silicon (blue).

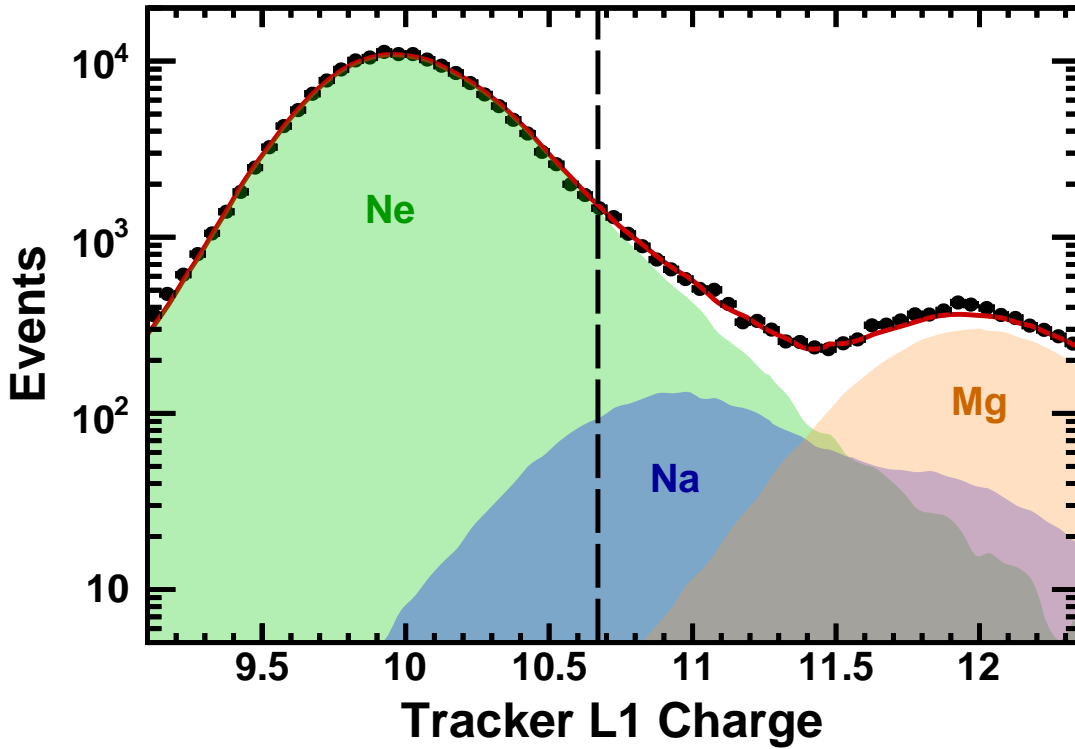


FIG. S2. Charge distributions measured by tracker $L1$ for neon events selected by the inner tracker in the rigidity range between 9 and 11 GV (black dots). The solid red curve shows the fit to the data of the Ne, Na and Mg charge distribution templates. The templates are obtained from non-interacting samples at $L2$ by the use of the charge measurement with $L1$, upper TOF, and $L3-L8$. The charge selection applied on tracker $L1$ is shown as vertical dashed line. After selection, the residual Na background is found to be $<0.3\%$.

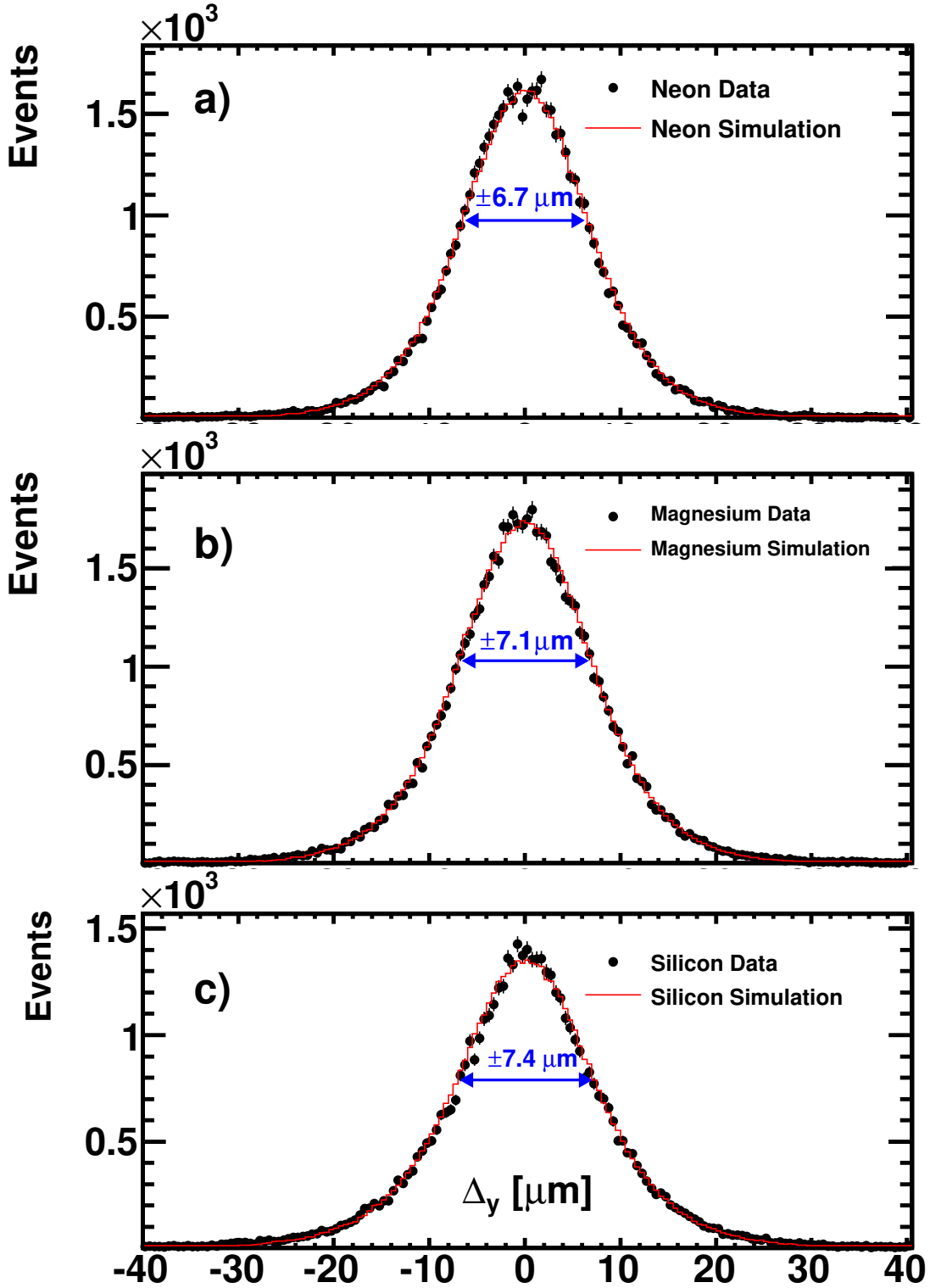


FIG. S3. Comparison of the differences of the coordinates measured in $L3$ or $L5$ to those obtained from the track fit using the measurements from $L1$, $L2$, $L4$, $L6$, $L7$, and $L8$ between data and simulation in the rigidity range $R > 50$ GV for (a) neon, (b) magnesium, and (c) silicon nuclei. The observed bending coordinate accuracy is $6.7 \mu\text{m}$ for neon, $7.1 \mu\text{m}$ for magnesium and $7.4 \mu\text{m}$ for silicon.

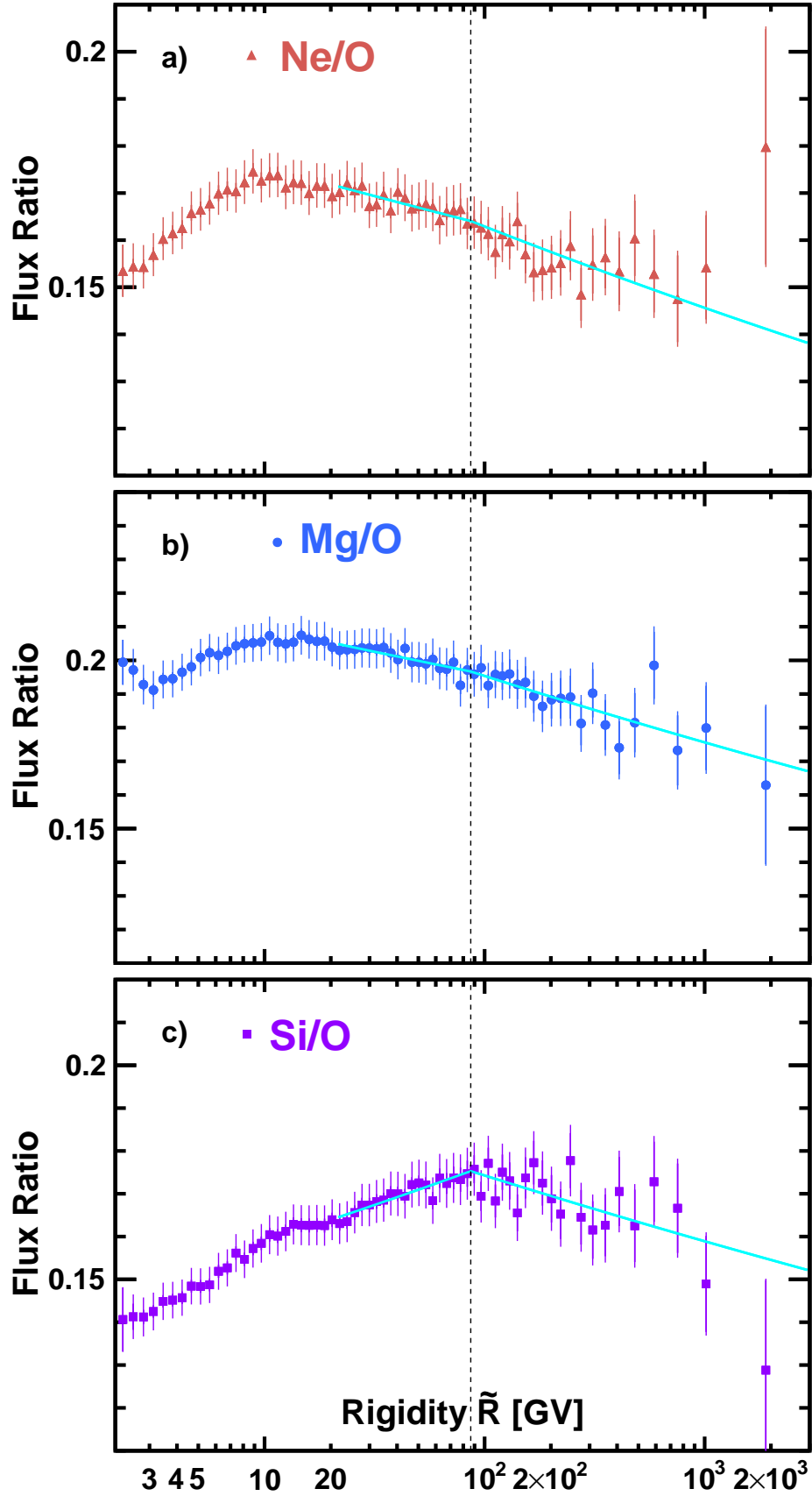


FIG. S4. The AMS a) Ne/O, b) Mg/O, and c) Si/O ratios as functions of rigidity. The solid lines indicate the fits of Eq. (4) for rigidities above 20 GV with $\chi^2/\text{d.o.f.} = 16/38$, $19/38$ and $27/38$ for Ne/O, Mg/O, and Si/O, respectively. The vertical dashed lines are placed at 86.5 GV which separates two fit interval of Eq. (4).